

The Design of a Neutron Generator Using the Inertial Electrostatic Confinement of Deuterium Plasma

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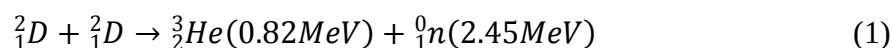
An Undergraduate Level Submission

Summary

A neutron generator was designed that uses the inertial electrostatic confinement (IEC) of a deuterium-based plasma to generate neutrons by the process of fusion. A two-stage high-vacuum system was designed that uses a rotary-vane pump and turbo-molecular pump. A pressure measurement system was designed that uses a Pirani pressure-gauge and an ionization pressure-gauge. A high-voltage system was designed that uses an off-the-shelf high voltage power supply and a Cockcroft-Walton voltage-multiplier circuit. A neutron detection system was designed that uses a Helium-3 neutron detector. Safety considerations in the operation of the device are discussed. It is expected this device is to be constructed in 2013-2014.

1. Introduction

The Inertial Electrostatic Confinement device is a system that uses electrostatic fields to accelerate and confine ions. The electrostatic field in a spherical IEC device is created by high voltage spherical wire-frame electrodes (an inner negative cathode and a positive outer anode). One use of such a device is the production of neutrons via the DD fusion reaction (see equation 1).



The theoretical principal behind IEC is as follows: the reaction chamber is initially filled with a high purity gas, such as deuterium, to undergo fusion. This gas should be kept at a low pressure so that its behaviour is primarily dictated by molecule-wall collisions (IE its pressure should be in the molecular flow regime or about 10^{-2}Torr^1 in the designed system). An extremely high, negative voltage (in the order of tens of kilo-Volts) is applied to the inner cathode while a high positive voltage (in the order of hundreds of Volts) is applied to the outer anode. There is a small fraction of background ionization of the reactant gas inside the chamber due to cosmic ray interactions². The deuterium ions from this initial ionization are attracted towards the inner cathode while the electrons are attracted towards the outer anode. The movement of these initial

¹ 1 Torr is defined to be $1/760^{\text{th}}$ of atmospheric pressure, $\sim 133.332\text{ Pa}$ or $\sim 1\text{mmHg}$

² In larger system running at lower pressures, the fraction of initial ionization is so small that other means such as ion guns or electron emitters must be used. See [9].

ions ionize the gas atoms along their path (much of the ionization will be due to electron bombardment of the deuterium gas) until the entirety of the gas is turned into plasma. Neglecting interactions with other ions, as an approximation, the energy acquired by the deuterons as they transverse the space between the anode and cathode is equal to the difference in electrical potential between the anode and cathode. The deuterons that miss the cathode collect in the focus of the cathode and create a region of higher density ions and electrons. When a deuteron is incident on this region of higher density ions and electrons, there is a probability that it will interact with deuterium ions trapped in the focus of the potential well with enough energy to tunnel through the Coulomb barrier and undergo nuclear fusion.

The essential components of an IEC device are: high-vacuum, high-voltage, and neutron detection. The high-vacuum system is used to evacuate the reaction vessel of any air and then back-fill it with reactant gas. The high-voltage system is used to apply high-voltage to the electrodes. The neutron detection system is used to detect any neutrons produced.

2. Overview of Design

The IEC device designed uses a two-stage high-vacuum system that is measured in a two-stage vacuum measurement system. In the design, deuterium is supplied via an external storage tank through a regulated valve. The DDn reaction itself is to occur within a six way Conflat cross [1] with glass viewports. The high negative voltage for the inner cathode is to be provided by a multi-stage Cockroft-Walton voltage-multiplier circuit [2]. High positive voltage is to be provided with an off-the-shelf high voltage power supply. Neutron detection in the design is to be accomplished with a Helium-3 neutron detector.

3. High Vacuum System

In the design, the whole high-vacuum system (Figure 1) is isolated into three sections: the vacuum back-end; the gas and measurement section; and, the reaction chamber. Each of these sections is isolated by a valve.

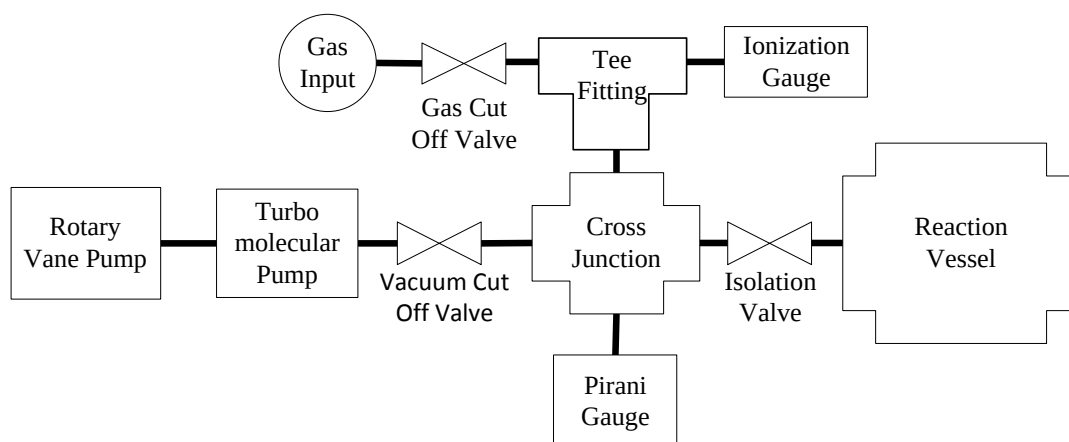


Figure 1: Diagram of the High Vacuum System

In the vacuum back-end, the system is to use two stages of pumping to reach pressures in the high vacuum regime. The first stage is a VIOT VDP5 [3] dual-stage rotary-vane pump [4] that lowers system pressure to 10^{-2} Torr. The second stage is a Leybold Turbovac 151 [5] turbomolecular pump [4] that is capable of an ultimate pressure of 10^{-9} Torr. It is unlikely that an ultimate system pressure of 10^{-9} Torr will be reached due to system leakage.

The rotary-vane pump is to connect to the turbomolecular pump via a wire-reinforced polyvinyl chloride (PVC) vacuum hose. The turbomolecular pump is to be water cooled by a water pump connected to a water reservoir.

In the measurement section, pressures ranging from atmospheric pressure to 10^{-4} Torr are to be measured with a Gransville-Phillips 275 Mini-Convectron [6] Pirani pressure-gauge [4]. To cover the full range of measurable pressures, the Pirani pressure-gauge divides its output signal into three distinct voltage regimes. Pressure readings from the Pirani pressure-gauge are to be read by an Arduino Microcontroller [7] through a voltage divider. Pressures ranging from 10^{-4} Torr to 10^{-9} Torr are to be measured using a Gransville-Phillips 271 ionization pressure-gauge [4] and controller. The ionization pressure-gauge is to be fitted into a DN40 Conflat tee fitting. This tee fitting is to be attached to a four-way DN40 Conflat cross that will also hold the Pirani pressure-gauge. Copper gaskets are to be used on all Conflat fittings.

The reaction chamber will be a six-way DN160 Conflat cross. The Conflat cross is to be fitted with a viewport. The high voltage feed-troughs are to be installed on the top and bottom of the Conflat cross such that the cathode will be supported from the bottom and the larger anode will hang from top. The DN160 Cross is to be fitted to a DN160-DN40-DN63 Conflat Tee with a blank flange installed on the DN63 end. The measurement section is to be attached to the reaction chamber on the DN40 section of the Conflat Tee via a DN40 Conflat connection. Blanks are to be installed on the rest of the ports of the cross. A gas feed system is to be installed into the vacuum boundary by a 1/4" NPT brass globe valve attached to an adapter on the DN-40 Tee

fitting. To prevent leakage, the threads of the NPT fitting are to be sealed with the Hysol 1C: a vacuum grease that is rated down to 10^{-9} Torr.

4. High Voltage System

The high-voltage system is to consist of a high-voltage negative out, positive ground power supply; a high voltage positive out, negative ground power supply; and two spherical stainless steel electrodes (see Figure 2).

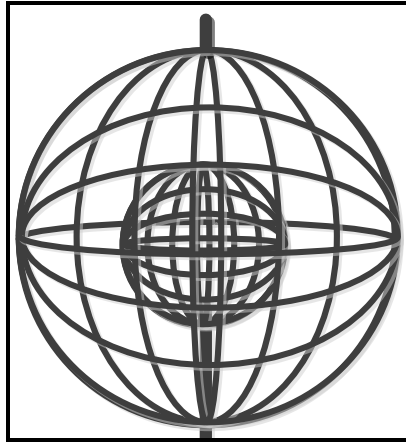


Figure 2: Drawing of the spherical electrodes used in IEC

The high-voltage negative out, positive ground power supply is to be rated to 25kV and is to be built from a 2kV gas sign transformer attached to a five stage Cockcroft-Walton voltage multiplier circuit using 5kV ceramic capacitors. This configuration enables very high voltage, low current power to be supplied to the inner cathode. The high-voltage positive out, negative ground power supply is from an Ortec 556 [8] power supply set to a voltage of 400 Volts.

The electrodes are to be built from 1/8" stainless-steel wire that will be Metal-Inert-Gas (MIG) welded into a shape such as the one shown in figure two. Stainless-steel rod will connect the electrodes to the high voltage feed through and act as mechanical support for the electrodes.

5. Neutron Detection System

Neutron detection will be done through a Helium-3 detector positioned outside of the reaction chamber. The detector will be encased in paraffin blocks that will thermalize any neutrons entering the detector and thereby increase their probability of detection. A neutron detection rate that is above the background detection rate is evidence that the DDn reaction is occurring.

6. Safety Considerations

Given that IEC devices operate at high voltages, certain precautions must be taken to ensure safe operation. Issues that require attention are: high-voltage, radiation, and deuterium combustion.

High voltage safety will be ensured by using high-voltage test equipment on all diagnostic equipment. Grounding straps and rubber mats are to be used when any work needs to be done on high voltage equipment. Capacitors will be discharged via a short circuit between the terminals with a high resistance bleed resistor. A protective shield will surround the Cockcroft-Walton voltage multiplier circuit when in operation.

Radiation from the IEC device will be in two forms: X-rays and neutrons. The X-ray production comes from bremsstrahlung reactions produced inside of the plasma, and also from energetic electrons bombarding the structural materials. Neutrons are produced through DDn reactions. To address radiation safety, experiments will be performed inside of an isolated, shielded facility with no humans present. The high-voltage power will be turned on remotely so that the system can operate with no humans present. A video camera will be set up in the view port so that the reaction can be viewed.

It is understood that deuterium gas is flammable, and precautions will be taken to prevent combustion by ensuring that there is no oxygen within the reaction chamber. However, it is also recognized that the system operates at low pressure (10^{-2} Torr of deuterium), and the combustion energy potential is relatively low. From a combustion perspective, the IEC device, is likely safer than operating an acetylene torch. Potential safety concerns from combustion of deuterium gas will be addressed by ensuring the operating room is evacuated when the device is at power.

7. Conclusion

The preliminary design for a device which uses the inertial electrostatic confinement of deuterium ions to generate neutrons has been completed. It is expected that this device will be constructed at the University of Ontario Institute of Technology (UOIT) in 2013-2014. Equipment procurement is ongoing. Initial testing will be performed by using inert helium followed later by the use of hydrogen gas. It is expected that when operating at full capacity, the device will produce somewhere in the range of 100,000 neutrons per second. It is anticipated that an operating license from the Canadian Nuclear Safety Commission (CNSC) will be required to licencing will be required to use deuterium gas in the UOIT-IEC Mark I device.

8. References

- [1] Kurt J. Lester Company “CF Flanges” (online)
http://www.lesker.com/newweb/flanges/flanges_technicalnotes_conflat_1.cfm?pgid=0 April 25, 2013
- [2] J. Kuffel, E. Kuffel, W.S. Zaengl “Cascade Circuits” in “High Voltage Engineering Fundamentals” Newnes, 2000, pp. 13-21
- [3] VIOT (online) <http://viot.us/> April 25, 2013

- [4] John F. O’Hanlon “*A User’s Guide to Vacuum Technology*” Third Edition, John Wiley and Sons, 2003
- [5] OerlikonLeybond Vacuum Company (online)
<http://www.oerlikon.com/leyboldvacuum/en/> April 25, 2013
- [6] Brook Automation (parent company of Gransville-Phillips) (online)
<http://www.brooks.com/> April 25, 2013
- [7] Arduino (online) <http://www.arduino.cc/> April 25, 2013
- [8] Ortec (online) <http://www.ortec-online.com/> April 25, 2013
- [9] Philo T. Farnsworth et. al. “*Method and Apparatus for Producing Nuclear-Fusion Reactions*”, U.S. Patent 3386883, May 13 1966.
- [10] Hirsch, R. Meek, G. “*Apparatus for Generating Fusion Reactions*” US Patent 3530036 issued September 22, 1970
- [11] Andrew Seltzman “*Design of an Actively Cooled Grid System To Improve Efficiency in Inertial Electrostatic Confinement Fusion Reactors*”, Master’s Thesis, Georgia Institute of Technology, Atlanta Georgia, 2008.
- [12] Andrew Sesselmann. “*Reactor for Producing Controlled Nuclear Fusion*” Australian Patent PCT/AU2011/000604, 2006.
- [13] Thomas Dolan “*Fusion Research: Principals, Experiments and Technology*”, Pergamon Press, Oxford 1981.
- [14] The Fusor Online Community at <http://www.fusor.net>

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