

Theoretical Research of Weak Neutron Source Induced Bursts in Fast Neutron Reactor

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Abstract

We find that theoretical calculation using Hansen's model is significantly different from experimental results of weak source induced bursts by Wimett et al. on Godiva-II. Based on solution of the probability of n neutrons at time t , the expected length of finite fission chain is evaluated and the multiplication of delayed neutron precursors is studied, which indicate that the number of delayed neutrons may vary several times during the waiting time. With consideration of the multiplication of delayed neutron precursors, an improved theoretical model of probability distributions of burst wait-time is presented, which consist well with experimental results of Godiva-II

1. Introduction

In slightly supercritical system in presence of weak source, such as reactor startup, critical safety analysis and pulse experiments, the stochastic behavior of neutrons during multiplication has attracted much attention for many years.

The stochastic behavior of neutrons had been shown by Wimett et al. on Godiva-II in 1960 [1], and was also confirmed on CFBR-II by the Institute of Nuclear Physics and Chemistry, China Academy of Engineering Physics.

Hansen studied this phenomena and developed a theoretical model [2] which has been used by many other researchers since then. However, we note that when the average waiting time in presence of weak source and the probability distributions in time of burst occurrence are calculated using Hansen's method, the consistency between calculations and experimental results is not good.

Wimett improved Hansen's model by introducing adjustable parameters in the formula of probability distributions in time of burst occurrence. However, since these free input parameters don't have definite physical meaning and must be calibrated by experiments, Wimett's method cannot be used to predict experiments.

This stochastic behavior was still not well understood till 2007, as pointed by Greenman, LLNL believed it is necessary to develop new code in order to simulate this behavior of neutrons in experiments.

We studied Hansen's model and found that the contributions of finite fission chains and delayed neutrons are ignored in his model, although these contributions have been discussed in his paper. Furthermore, the source strength during the waiting time and the probability of a source neutron sponsoring a persistent fission chain are also considered as constants in Hansen's model.

In this paper, we improve Hansen's model by solving the expectation of finite fission chain and the multiplication of delayed neutron precursors due to finite fission chain. The calculated results are in good agreement with the experimental data. Then we discuss the probability of a source neutron sponsoring a persistent fission chain. The probability equilibrium equation and its solution are given. In section III, deduction of the probability of extinction and sponsoring a persistent fission chain at time t is presented. We evaluate the expectation of the finite fission chain in section IV and give the calculated in section V with consideration of the multiplication of delayed neutron precursors. An improved theoretical model of probability distributions of burst wait-time is presented, which consist well with experimental results of Godiva-II in section VI.

2. Probability Equilibrium Equation $P_n(t_0, t)$ and its Solution

We consider a simple point reactor in which all neutrons behave identically, each neutron has the probability p of producing fission, each fission has the probability $p(\nu)$ of emitting ν neutrons. Let W be the probability of a source neutron sponsoring a persistent fission chain. Denote $P_n(t_0, t)$, the probability of a source neutron at time t_0 sponsoring n neutrons at time t , which satisfies the equation

$$\tau \frac{dP_n(t_0, t)}{dt} = (1-p)(n+1)P_{n+1}(t_0, t) - nP_n(t_0, t) + p \sum_{\nu=0}^{\infty} P(\nu)(n-\nu+1)P_{n-\nu+1}(t_0, t) \quad (1)$$

Here τ is the mean lifetime of a neutron. The initial condition of $P_n(t_0, t)$ is

$$P_n(t_0, t) = \delta_{nl} \quad \delta_{nl} = \begin{cases} 1 & n = l \\ 0 & n \neq l \end{cases} \quad (2)$$

where δ_{nl} is the Kronecker delta. Obviously $P_n(t_0, t)$ satisfies

$$\sum_{n=0}^{\infty} P_n(t_0, t) = 1. \quad (3)$$

By introduction of parameter z , the generation function of $P_n(t_0, t)$ can be defined as

$$G(z; t_0, t) = \sum_{n=0}^{\infty} P_n(t_0, t) z^n \quad (4)$$

From eq. (4) we can derive $P_n(t_0, t)$,

$$P_n(t_0, t) = \frac{1}{n!} \left. \frac{d^n G(z; t_0, t)}{dz^n} \right|_{z=0} \quad (5)$$

Multiply both sides of eq. (1) with Z^n and make a summation for n we can get the equation satisfied by $G(z; t_0, t)$,

$$\tau \frac{\partial}{\partial t} G(z; t_0, t) = \left[p \left(\sum_{\nu} P(\nu) z^{\nu} - z \right) + (1-p)(1-z) \right] \frac{\partial}{\partial z} G(z; t_0, t) \quad (6)$$

The initial condition of eq. (6) is

$$G(z; t_0, t_0) = z \quad (7)$$

Then eq. (3) can be written as

$$G(1; t_0, t) = 1 \quad (8)$$

And the characteristic equation of (6) is

$$\tau \frac{dz}{dt} = -p \left(\sum_{\nu} P(\nu) z^{\nu} - z \right) - (1-p)(1-z) \quad (9)$$

From partial differential equation theory, we have $G(z; t_0, t) = z$. G should also satisfy the equation which is satisfied by z . Therefore, replacing t by t_0 and z by G in eq. (9), we can get

$$\tau \frac{d}{dt_0} G(z; t_0, t) = -p \left(\sum_{\nu} P(\nu) [G(z; t_0, t)]^{\nu} - G(z; t_0, t) \right) - (1-p)[1 - G(z; t_0, t)] \quad (10)$$

And the initial condition (7) becomes the final condition

$$G(z; t, t) = z \quad (11)$$

For convenience, let

$$W(z; t_0, t) = 1 - G(z; t_0, t) \quad (12)$$

Substitution of (12) into (10) yields

$$\tau \frac{d}{dt_0} W(z; t_0, t) = p \left\{ \sum_{\nu} P(\nu) [1 - W(z; t_0, t)]^{\nu} - 1 \right\} + W(z; t_0, t). \quad (13)$$

Eq. (11) becomes

$$W(t, t; z) = 1 - z \quad (14)$$

And the normalization condition becomes

$$W(1; t_0, t) = 0 \quad (15)$$

For a slightly supercritical system, where $W \ll 1$ is satisfied, the term

$(1 - W(z; t_0, t))^{\nu}$ may be approximated as

$$(1 - W)^{\nu} \approx 1 - \nu W + \frac{1}{2} \nu(\nu - 1) W^2 \quad (16)$$

Substitute (16) into (13), and note $\sum_{\nu=0} p(\nu) = 1$, we have

$$\frac{d}{dt_0} W(z; t_0, t) = -\alpha W(z; t_0, t) + \frac{1}{2} p \overline{\nu(\nu-1)} W^2(z; t_0, t) \frac{1}{\tau} \quad (17)$$

Utilizing $\alpha = \frac{1}{\tau}(k-1)$; $\bar{\nu} = \sum_{\nu} P(\nu)\nu$; $\overline{\nu(\nu-1)} = \sum_{\nu} P(\nu)\nu(\nu-1)$; $\Gamma_2 = \overline{\nu(\nu-1)}/\bar{\nu}^2$, we can

rewrite (17) as the linear equation of $\frac{1}{W(z; t_0, t)}$

$$\frac{d}{dt_0} \frac{1}{W(z; t_0, t)} = \frac{\alpha}{W(z; t_0, t)} - \frac{\Gamma_2 \bar{\nu}^2}{2} p \frac{1}{\tau} \quad (20)$$

The solution is

$$W(z; t_0, t) = \frac{e^{\alpha(t-t_0)}}{\frac{\Gamma_2 \bar{\nu}^2}{2} p \frac{1}{\tau \alpha} (e^{\alpha(t-t_0)} - 1) + \frac{1}{1-z}} \quad (21)$$

which can be further rewrote as

$$W(z; t_0, t) = \frac{\varepsilon}{\eta} \frac{z-1}{z - \left(1 + \frac{1}{\eta}\right)} = \frac{\varepsilon}{1+\eta} \left[1 - \frac{1}{\eta} \sum_{n=1}^{\infty} \frac{z^n}{\left(1 + \frac{1}{\eta}\right)^n} \right] \quad (22)$$

Here

$$\varepsilon = e^{\frac{1}{\tau}(k-1)(t-t_0)} \quad (23)$$

$$\eta = \frac{\Gamma_2 \bar{\nu}^2}{2} p \frac{1}{\tau \alpha} (e^{\frac{1}{\tau}(k-1)(t-t_0)} - 1) \quad (24)$$

So we have

$$P_0(t_0, t) = 1 - \frac{\varepsilon}{1+\eta} \quad (25)$$

$$P_n(t_0, t) = \frac{\varepsilon}{(1+\eta)\eta} \left(1 + \frac{1}{\eta}\right)^{-n} \quad (n \neq 0) \quad (26)$$

With $\alpha = \frac{1}{\tau}(k-1)$, $k = \bar{\nu}p$, $\bar{\nu}$ is the average number of neutrons emitted by one fission, (23) and (24) may be rewritten as

$$\varepsilon = e^{\frac{1}{\tau}(k-1)(t-t_0)} = e^{\alpha(t-t_0)} \quad (27)$$

$$\eta = \frac{\Gamma_2 \bar{\nu}}{2\rho} \left(e^{\frac{1}{\tau}(k-1)(t-t_0)} - 1 \right) = \frac{\Gamma_2 \bar{\nu}}{2\rho} (e^{\alpha(t-t_0)} - 1) \quad (28)$$

where $\rho = \frac{k-1}{k}$ is the prompt reactivity. Thus, as we can see from eq. (21), the probability W of a source neutron sponsoring a persistent fission chain is related to the prompt reactivity ρ and the mean lifetime τ of a neutron.

If we treat W as the probability of non-extinction, that is, $W = 1 - \lim_{t \rightarrow \infty} P_0(t_0, t)$.

Then, when $(t - t_0) \rightarrow \infty$, from eq. (22), (25) and (28), we can obtain

$$W(t_0, t \rightarrow \infty) = 1 - \lim_{t \rightarrow \infty} P_0(t_0, t) = 1 - \lim_{t \rightarrow \infty} \left(1 - \frac{\varepsilon}{1 + \eta} \right) = \lim_{t \rightarrow \infty} \left(\frac{\varepsilon}{1 + \eta} \right) = \frac{2}{\Gamma_2 \bar{V}} \rho \quad (29)$$

And (28) can be rewrote as

$$\eta = \frac{\Gamma_2 \bar{V}}{2\rho} (e^{\alpha(t-t_0)} - 1) = \frac{1}{W} (\varepsilon - 1) \quad (30)$$

When η is large enough, n in (1.28) can be considered as continuous, thus we have

$$P_n(t_0, t) = \frac{\varepsilon}{(1 + \eta)\eta} e^{-\frac{n}{\eta}} \quad (31)$$

The normalization condition is

$$P_0(t_0, t) + \int_0^\infty P_n(t_0, t) dn = P_0(t_0, t) + \int_0^\infty \frac{\varepsilon}{(1 + \eta)\eta} e^{-\frac{n}{\eta}} dn = 1. \quad (32)$$

The average neutron numbers can be obtained

$$\int_0^\infty n P_n(t_0, t) dn = \int_0^\infty n \frac{\varepsilon}{(1 + \eta)\eta} e^{-\frac{n}{\eta}} dn \approx \varepsilon = e^{\alpha(t-t_0)} = \bar{n}. \quad (33)$$

Since $(1 - W)^n W$ represents the probability of n neutrons not inducing persistent fission chain, while the $(n+1)^{\text{th}}$ neutron does, therefore, $\bar{n}$ is the expected value of n neutrons sponsoring a persistent fission chain, then we have

$$W + (1 - W)W + (1 - W)^2 W + \dots + (1 - W)^n W + \dots = W \sum_{n=0}^\infty (1 - W)^n = 1 \quad (34)$$

Thus we obtain the average number of neutrons required to sponsor a persistent fission chain in the system

$$\bar{n} = W \sum_{n=0}^\infty (n + 1) (1 - W)^n = \frac{1}{W} \quad (35)$$

3. The Probability of Extinction and Sponsoring a Persistent Fission Chain at Time T

We assume the first neutron is introduced into the system at $t_0 = 0$. And the probability of n neutrons sponsoring persistent fission chain is $1 - e^{-nW}$, where e^{-nW} is the probability of n neutrons not sponsoring persistent fission chain. Thus, $n \nu \Sigma_f P_n(t) (1 - e^{-nW}) dt$ is the contribution of the probability of n neutrons in the system to sponsoring a persistent fission chain in dt , whereas $n \nu \Sigma_f P_n(t) e^{-nW} dt$ is the contribution of the probability of n neutrons in the system to sponsoring a non-persistent fission chain in dt .

Define $P_0(t)$ as the extinction probability at time t , and assume there is already one neutron in the system at $t = 0$, thus $P_0(0) = 0$ is the initial condition. And we also have

$$P_1(0)e^{-W} = P_1(0)(1 - W) = 1 - W \quad (36)$$

$$P_1(0)(1 - e^{-W}) = P_1(0)W = W \quad (37)$$

$$P_{n \neq 1}(0) = 0 \quad (38)$$

$$P_n(t) = \frac{\varepsilon}{(1 + \eta)\eta} e^{-\frac{n}{\eta}} \quad (39)$$

where $\varepsilon = e^{\alpha}$, $\eta = \frac{1}{W}(e^{\alpha} - 1)$, $P_0(t) + \int_0^{\infty} P_n(t) dn = 1$.

The neutrons sponsoring persistent fission chain will not die out, that is

$$\int_0^{\infty} P_n(t) (1 - e^{-nW}) dn = P_1(0)(1 - e^{-W}) = W \quad (40)$$

The extinction probability at time t equals the probability of sponsoring non-persistent fission chain at the initial time minus these at time t , that is,

$$P_0(t) = (1 - W) - \int_0^{\infty} P_n(t) e^{-nW} dn \quad (41)$$

$$P_0(t) = 1 - \frac{\varepsilon}{1 + \eta} = 1 - \frac{e^{\alpha}}{1 + \frac{1}{W}(e^{\alpha} - 1)} \quad (42)$$

$$\begin{aligned} \int_0^{\infty} P_n(t) e^{-nW} dn &= \frac{\varepsilon}{(1 + \eta)\eta} \int_0^{\infty} e^{-\frac{n}{\eta}} e^{-nW} dn = \frac{\varepsilon}{(1 + \eta)\eta} \frac{1}{-\left(\frac{1}{\eta} + W\right)} \int_0^{\infty} e^{-\left(\frac{1}{\eta} + W\right)n} d\left[-\left(\frac{1}{\eta} + W\right)n\right] \\ &= -\frac{e^{\alpha}}{1 + \frac{1}{W}(e^{\alpha} - 1)} \frac{1}{1 + e^{\alpha} - 1} = \frac{1}{1 + \frac{1}{W}(e^{\alpha} - 1)} \end{aligned} \quad (43)$$

$$\int_0^{\infty} P_n(t) dn = \int_0^{\infty} \frac{\varepsilon}{(1 + \eta)\eta} e^{-\frac{n}{\eta}} dn = -\frac{\varepsilon}{(1 + \eta)} \int_0^{\infty} e^{-\frac{1}{\eta}n} d\left(-\frac{1}{\eta}n\right) = \frac{\varepsilon}{(1 + \eta)} = \frac{e^{\alpha}}{1 + \frac{1}{W}(e^{\alpha} - 1)} \quad (44)$$

Substitution of (43) and (44) into (40) yields

$$\begin{aligned} \int_0^\infty P_n(t)(1 - e^{-nW})dn &= \int_0^\infty P_n(t)dn - \int_0^\infty P_n(t)e^{-nW}dn \\ &= \frac{e^{\alpha t}}{1 + \frac{1}{W}(e^{\alpha t} - 1)} - \frac{1}{1 + \frac{1}{W}(e^{\alpha t} - 1)} = \frac{e^{\alpha t} - 1}{1 + \frac{1}{W}(e^{\alpha t} - 1)} = \frac{W}{\frac{W}{e^{\alpha t} - 1} + 1} \approx W \quad (45) \end{aligned}$$

which is satisfied under the condition $W/(e^{\alpha t} - 1) \ll 1$, or $(e^{\alpha t} - 1) \gg W$.

From the experimental data of Godiva-II, $W \approx 10^{-3}$, and the above condition requires $\alpha t \gg 10^{-3}$ or $t \gg \frac{10^{-3}}{\alpha}$.

Apparently, $t < \frac{10^{-3}}{\alpha}$ is a very short amount of time, which is also the requirement in the

deduction of the continuous form of $P_n(t_0, t)$, where $\frac{1}{\eta} \ll 1$, or $W/(e^{\alpha t} - 1) \ll 1$ is required.

From (42) and (43), we obtain the left side of eq. (41)

$$P_0(t) = 1 - \frac{e^{\alpha t}}{1 + \frac{1}{W}(e^{\alpha t} - 1)}, \quad (46)$$

and the right side of eq. (41)

$$\begin{aligned} 1 - W - \int_0^\infty P_n(t)e^{-nW}dn &= 1 - W - \frac{1}{1 + \frac{1}{W}(e^{\alpha t} - 1)} \\ &= 1 - \frac{W + e^{\alpha t}}{1 + \frac{1}{W}(e^{\alpha t} - 1)} \quad (47) \end{aligned}$$

respectively. We note that $e^{\alpha t} \gg W$ is satisfied for Godiva-II, thus (46) equals (47) approximately. Therefore, eqn. (41) is verified.

4. Expectation of Finite Fission Chain Length $\langle n_f \rangle$

Let us consider a point reactor and ignore all delayed neutrons, assume one neutron is introduced into the system at the starting point which sponsors a non-persistent fission chain. Then the average number of fissions $\langle n_f \rangle$ is defined as the expectation of the finite fission chain length.

As defined in section III, e^{-nW} is the probability of n neutrons not sponsoring persistent fission chain, and $n\nu\sum_f P_n(t)e^{-nW}dt$ is the contribution of the probability of n neutrons in the system sponsoring a non-persistent fission chain in dt , we have

$$\langle n_f \rangle = \int_0^\infty dn \int_0^\infty n\nu P_n(t)e^{-nW}dt \quad (48)$$

First do the integration over t ,

$$H = n \nu \Sigma_f e^{-nW} \int_0^\infty \frac{\varepsilon}{(1+\eta)\eta} e^{-\frac{n}{\eta}} dt. \quad (49)$$

let $y = \frac{1}{e^{\alpha} - 1}$, then $e^{\alpha} = \frac{1}{y} + 1$; $de^{\alpha} = -\frac{1}{y^2}$; $\eta = \frac{1}{W}(e^{\alpha} - 1) = \frac{1}{W} \frac{1}{y}$; $\frac{1}{\eta} = Wy$.

Substitution of above equations into (49) yields

$$\begin{aligned} H &= n \nu \Sigma_f e^{-nW} \int_0^\infty \frac{e^{\alpha}}{1 + \frac{1}{W}(e^{\alpha} - 1)} e^{-\frac{nW}{e^{\alpha} - 1}} \frac{W}{e^{\alpha} - 1} dt \\ H &= \int_0^\infty \left(-\frac{dy}{y^2} \right) e^{-nWy} \frac{1}{\alpha} (Wy)^2 (\Sigma_f \nu e^{-nW}) = \frac{1}{\alpha} W^2 (\Sigma_f \nu e^{-nW}) \int_0^\infty e^{-nWy} dy \\ &= \frac{1}{\alpha} W^2 \Sigma_f \nu e^{-nW} \left(\frac{-1}{nW} \right) e^{-nWy} \Big|_0^\infty = \Sigma_f \nu \frac{W}{\alpha} e^{-nW} \end{aligned} \quad (50)$$

Here the condition $\frac{1}{\eta} \ll 1$ has been applied.

as $\alpha = \bar{\nu} \Sigma_f \nu \rho$, eq. (50) can be rewritten as

$$H = \Sigma_f \nu \frac{W}{\alpha} e^{-nW} = \frac{1}{\bar{\nu} \rho} W e^{-nW}. \quad (51)$$

And the eq. (48) becomes

$$\langle n_f \rangle = \int_0^\infty H dn = \int_0^\infty \frac{1}{\bar{\nu} \rho} W e^{-nW} dn = \frac{1}{\bar{\nu} \rho} [-e^{-nW}]_0^\infty = \frac{1}{\bar{\nu} \rho} \quad (52)$$

If the upper limit of the neutron numbers is n , the expectation is

$$\langle n_f \rangle_n = \int_0^n H dn = \frac{1}{\bar{\nu} \rho} (1 - e^{-nW}). \quad (53)$$

If $n = \frac{1}{W}$, then $\langle n_f \rangle_n = \frac{1}{\bar{\nu} \rho} 0.632$. That is, from $n=0$ to $\bar{n} = \frac{1}{W}$, the contribution of the

neutrons to the finite fission chain is 63.2%; the contribution of the neutrons from $\bar{n} = \frac{1}{W}$ to

$\bar{n} = \infty$ is 36.8%.

In eq. (48), if we first do the integration over n , let

$$\begin{aligned} G &= \Sigma_f \nu \int_0^\infty n P_n(t) e^{-nW} dn = \Sigma_f \nu \int_0^\infty \frac{\varepsilon}{(1+\eta)\eta} e^{-\left(\frac{1}{\eta} + W\right)n} dn \\ &= \Sigma_f \nu \frac{\varepsilon}{(1+\eta)\eta} \frac{1}{\frac{1}{\eta} + W} \left[-n e^{-\left(\frac{1}{\eta} + W\right)n} \right]_0^\infty + \Sigma_f \nu \frac{\varepsilon}{(1+\eta)\eta} \int_0^\infty n \frac{e^{-\left(\frac{1}{\eta} + W\right)n}}{\frac{1}{\eta} + W} dn \\ &= \Sigma_f \nu \frac{\varepsilon}{(1+\eta)\eta} \frac{1}{\left(\frac{1}{\eta} + W\right)^2} \end{aligned} \quad (54)$$

Substitute (54) into (48), we have

$$\begin{aligned}\langle n_f \rangle &= \int_0^\infty dt G = \Sigma_f \nu \int_0^\infty dt \frac{\varepsilon}{(1+\eta)\eta} \frac{1}{\left(\frac{1}{\eta} + W\right)^2} \\ &= \Sigma_f \nu \int_0^\infty dt \frac{e^{\alpha t}}{e^{2\alpha t}} = \Sigma_f \nu \int_0^\infty dt e^{-\alpha t} = \frac{\Sigma_f \nu}{\alpha} = \frac{1}{\bar{\nu} \rho}.\end{aligned}\quad (55)$$

Here $\frac{\eta}{(1+\eta)} \approx 1$ is assumed. Let $\langle n_f \rangle = \Sigma_f \nu \int_0^T dt e^{-\alpha t} = \frac{1}{\nu \rho} (1 - e^{-\alpha T})$, $\alpha T = 3$,

then $\langle n_f \rangle_{\alpha T=3} = \frac{1}{\bar{\nu} \rho} 0.95$ which means the relaxation time of forming a finite fission chain is

$T = \frac{3}{\alpha}$. The physical meaning of eq. (52) is manifest, for $\rho \ll 1$, $\langle n_f \rangle$ is inversely proportion to $\bar{\nu} \rho$.

Now we can evaluate the expectation of the fission numbers of finite fission chain. Given $\beta_{\text{eff}}=0.0069$, $\bar{\nu}=2.59$, $\Gamma_2=0.795$, $\rho (\$)=0.05$ for Godiva-II, the expectation is $\langle n_f \rangle \approx 1119$ which is well consistent with $\langle n_f \rangle \approx 1200$ from Spriggs [3].

5. Delayed Neutron Precursors Equation and Its Solution

Under the point reactor model, the differential equations for the slow development of the delayed neutron precursor due to the finite fission chain are considered as;

$$\frac{dC_i(t)}{dt} = -\lambda_i C_i(t) + [S_0 + \sum_{i=1}^6 \lambda_i C_i(t)] \bar{\nu} \beta_i \langle n_f(t) \rangle \alpha_i \quad (56)$$

$$\sum_{i=1}^6 \alpha_i = 1 \quad (57)$$

Among them, $C_i(t)$ is fraction of the delayed neutrons precursors, the i group; λ_i is the constant disintegration of the i group of delayed neutrons precursors fraction, $\langle n_f(t) \rangle$ is the mathematical expectation of the fission times of a source neutron and its progeny, S_0 is the Spontaneous fission source and initial delayed neutron source

In $S_0 = S_{sf} + S_d$, S_{sf} is the spontaneous fission source for the device, S_d is the Delayed neutron source. If there is the delayed neutron in the initial system S_d , The spontaneous fission neutron can be regarded as the initial source S_0 .

According to the formula (56), it is known that the $\langle n_f(t) \rangle$ slow variation of the neutron with time is related to the expectation of the finite length fission chain. When the formula (1) is made of a single group of delayed neutrons, the neutron source in the system can be expressed as:

$$S(t) = S_0 + \xi C(t) \quad (58)$$

Among them, the mathematical expectation of the concentration of the precursor is the average decay constant of the single group.

$C(t)$ will meet the following differential equation;

$$\frac{dC(t)}{dt} = -\xi C(t) + [S_0 + \xi C(t)] \bar{\nu} \beta_{eff} \langle n_f(t) \rangle \quad (59)$$

Obviously, it is also needed to consider prompt reactivity ρ_p and the delayed reactivity of finite fission chain expectation value contribution, therefore, $\langle n_f(t) \rangle$ meet the following relationships:

$$\langle n_f(t) \rangle = \frac{1}{\bar{\nu} \rho_p + \bar{\nu} \beta_{eff} (1 - e^{-\xi t})} \quad (60)$$

Handle (60) into equation (59) obtained

$$\frac{dC(t)}{dt} = -\xi C(t) + [S_0 + \xi C(t)] \frac{\beta_{eff}}{\rho_p + \beta_{eff} (1 - e^{-\xi t})} \quad (61)$$

If the initial system does not slow the neutrons, so there are initial conditions

$$C(t=0) = 0 \quad (62)$$

Solving equation (61), and obtained by the initial condition (62)

$$C(t) = \frac{\beta_{eff}}{\xi \rho_p} (1 - e^{-\xi t}) S_0 \quad (63)$$

Handle (63) into equation (58) obtained

$$S(t) = S_0 \left[1 + \frac{\beta_{eff}}{\rho_p} (1 - e^{-\xi t}) \right] \quad (64)$$

Formula (64) shows the variation of the time of the system under the assumption of the point reactor model and the single group delayed neutron, proved that:

$$\xi = \xi_1 = \sum_{i=1}^6 \lambda_i \alpha_i \quad (65)$$

According to the ^{235}U fast fission neutron table data ^[3], the ξ value of the Godiva-II is:

$$\xi = \sum_{i=1}^6 \lambda_i \alpha_i \approx 0.4058 \quad (66)$$

Table 1 data of delayed neutrons from fast neutron induced ^{235}U fission

组号	1	2	3	4	5	6	$\sum_i$
λ_i	0.0127	0.03151	0.1171	0.3108	1.37	3.83	
$T_{1/2i}$	54.60	22.0	5.92	2.23	0.506	0.181	
a_i	0.039	0.235	0.207	0.381	0.114	0.024	1.0
$a_i \lambda_i$	4.953(-4)	7.4048(-3)	2.424(-2)	0.1184	0.15618	9.912(-2)	0.4058

According to the formula (64) and the experimental parameters, the proliferation of delayed neutrons in the waiting time of the pulse is calculated.

For example: When the $t = 0$, $S(0) = S_0$.

The results of delayed neutron multiplication with the proliferation of Godiva-II were included in Table 2 during the waiting period.

Table 2 the proliferation data of delayed neutron in Godiva-II reactor

t(sec)	0	1	2	3	4	5	6	7	8
S(t)(1/sec)	90	690	1090	1357	1653	1732	1732	1784	1820

When the waiting time $t \rightarrow \infty$:

$$S(t) = S_0 \left[1 + \frac{\beta_{eff}}{\rho_p} \right] \quad (67)$$

The experimental parameter of Godiva-II given by the Wimett $\beta_{eff} = 0.0069$, $\rho_p = 0.05$, $S_0 = S_{sf} \approx 90/\text{sec}$ the source of the source of strength.

According to the experimental parameters, and formula (68), the maximum can be calculated to increase the system's delayed neutrons to more than 20 times.

Known, the Godiva-II experiment $\rho_p = 0.05$ (\$), we can obtain a source neutron that initiates a probability of a continuous fission chain;

$$W \cong \frac{2\rho}{\bar{\nu}\Gamma_2\eta} = \frac{2\rho}{\bar{\nu}\Gamma_2 1.48} \approx 0.00022642 \quad (68)$$

The average waiting time of the known Godiva-II experiment is about 3 seconds, according to the Hansen definition:

$$\bar{t}_1 = \frac{1}{WS} \quad (69)$$

The strength of the neutron source can be calculated in the moment of the system is about to be:

$$S(\bar{t}_1) = \frac{1}{W\bar{t}_1} \approx \frac{1}{0.002264 \times 3\text{sec}} \approx 1472/\text{sec}$$

This is very close to the results of the theoretical calculations in Table 2 for $t \approx 3$ seconds $S(t=3) \approx 1357/\text{sec}$

All the above analysis shows that the calculated results are in accordance with the experimental results.

6. Hansen Model Improve and Validate

The probability distribution model of waiting time probability distribution of pulsed reactor weak source is given under the assumption of step approximation of Hansen.

$$P_{1st}(t_1)dt_1 = \exp(-WSt_1)WSdt_1 \quad (70)$$

Apparently, according to the Hansen assumes, that the probability of a continuous fission chain W 、 ρ 、 S are all constant during the waiting period.

Obviously, Wimett found application Hansen model cannot simulate the good weak Godiva-II source outbreak pulse probability distribution curves, so Wimett in based on the Hansen model

(70) by is introduced to adjust the parameters of the gamma method can well simulate the experimental curve.

$$P_{1st}(N, t_1)dt_1 = WSdt_1 e^{-WS t_1} (1 - e^{-\gamma t_1}) \exp[-WS(1 - e^{-\gamma t_1})/\gamma] \quad (71)$$

Which γ is used as the main adjustment parameter of the curve shape. However, the Wimett method needs to be debugged according to the experimental results, cannot predict the experimental results, and cannot objectively reveal the actual physical phenomenon, so the method is not ideal.

After the previous discussion, we think that the delayed neutrons will be in the system during the waiting period. This will cause W to change, that is $\rho = \rho(t)$ 、 $W = W(t)$. Therefore, the Hansen model (70) can be rewritten as;

$$P_{1st}(t_1)dt_1 = W(t_1)S(t_1)dt_1 \exp\left[-\int_0^{t_1} W(t)S(t)dt\right] \quad (72)$$

Formula (72) and formula (70) is different, here is a source of strength, is a function of time. Obviously, formula (72) is difficult to obtain analytical solution directly. In order to solve, this order, then formula (72) can be expressed as

$$P_{1st}(t_1)dt_1 = F(t_1)dt_1 \exp\left(-\int_0^{t_1} F(t)dt\right) \quad (73)$$

$F(t)$ Can be written as

$$F(t) = W(t)S(t) = W_0 S_{cv}(t) = W_{cv}(t)S_0 \quad (74)$$

Formula (74), $S_{cv}(t)$ can be referred to as the equivalent source; W_0 is the probability of a continuous fission chain triggered by a neutron of source, $W_{cv}(t)$ is the equivalent probability of a continuous fission chain triggered by a neutron of source, S_0 called the constant source. Might as well assume:

$$F(t) = W_0 S_{cv}(t) \quad (75)$$

The implication is that the spontaneous fission neutron and delayed neutron is equivalent to neutron source. The type (75) into equation (73)

$$\begin{aligned} P_{1st}(t_1)dt_1 &= F(t_1)dt_1 \exp\left(-\int_0^{t_1} F(t)dt\right) \\ &= W_0 S_{cv}(t_1)dt_1 \exp\left[-\int_0^{t_1} W_0 S_{cv}(t)dt\right] \end{aligned} \quad (76)$$

Before previous chapter 1. We've got slow neutron $S_{cv}(t)$ expressions (64), formula (64) direct substitution type (76), and pay attention to this point, $W_0 \cong \frac{2\rho_p}{\beta\Lambda_2}$, we can get improved Hansen burst probability distribution model for:

$$P_{1st}(t_1)dt_1 = dt_1 S_0 \left[\frac{2}{\bar{\nu}\Gamma_2} (\rho_p + \beta_{eff}) - \frac{2}{\bar{\nu}\Gamma_2} \beta_{eff} e^{-\xi t_1} \right] \times \exp \left[-S_0 \left(\frac{2}{\bar{\nu}\Gamma_2} (\rho_p + \beta_{eff}) \right) t_1 + S_0 \frac{1}{\xi} \frac{2}{\bar{\nu}\Gamma_2} \beta_{eff} (1 - e^{-\xi t_1}) \right] \quad (77)$$

Using the formula (77) and the experimental parameters, the fitting curve and the experimental results are satisfactory, as shown in Figure

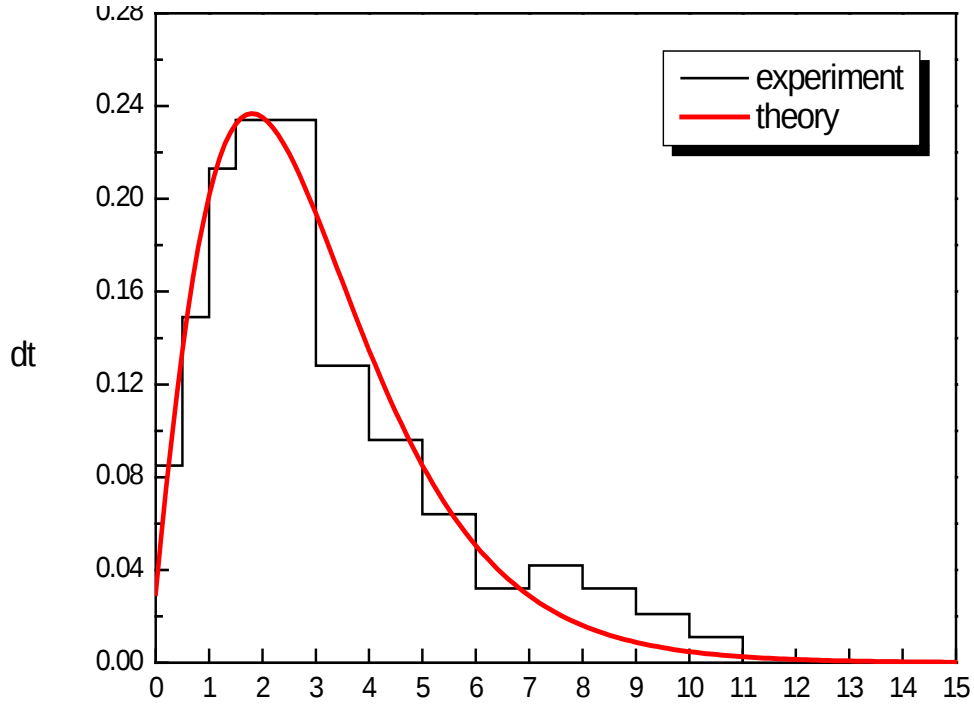


Fig. probability distribution curve of waiting time for Godiva reactor with 94 times

The expression of the average burst waiting time is given under the step approximation of Hansen.

$$\bar{t}_1 = \int_0^{\infty} t_1 P_{1st}(t_1) dt_1 \quad (78)$$

According to Table 3 experimental parameters in formula (77), (78) can be calculated by the average burst pulse time.

Table 3 pulse reactor parameters of Godiva- II							
	$\bar{\nu}$	ρ_p (\$)	B_{eff}	S_0/sec	Γ_2	n_f	ξ
Goiva-II	2.59	0.05	0.0069	90	0.795	1119	0.4058

The theoretical calculation of the average pulse duration of Godiva-II reactor

$$\bar{t}_1 = \int_0^{\infty} t_1 P_{1st}(t_1) dt_1 = 3.045 \text{秒}$$

The results are basically consistent with the experimental results of the average burst pulse time of Godiva-II reactor for 3 seconds.

7. Conclusion

In the study of fast neutron pulsed reactor weak source burst experiment, we found the limitations of Hansen model and method of the Wimett, Hansen model is improved by introducing the finite fission chain and delayed neutron precursors, the model can be very good description of the experimental results. The model is also applicable to other similar experiments of pulsed reactor.

8. References

- [1] T.F. Wimett, R.H. Whit, W.R. Stratton and D.P. Wood “Godiva- II An unmoderated Pulse-Irradiation Reactor” Nuc Sci. Eng 8,691(1960)
- [2] G.E. Hansen, Assembly of Fissionable Material in the Presence of Weak Neutron Source [J]. Nucl Sci. Eng. 1960, 8,709-719
- [3] G.D Spriggs et al The Equivalent Fundamental-Mode Source, Los Alamos Report LA-13253 (1997)
- [4] G.D Spriggs R.D. Busch and J.M. Campbell “Determination of Godivas Effective Delayed Neutron Fraction Using Newly Calculated Delayed Neutron spectra” Annual Meeting of the American Nuclear Society Boston, MA, 1999