### DEVELOPMENT AND THERMALHYDRAULIC CALCULATIONS OF A SCWR 64-ELEMENT FUEL BUNDLE

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#### Abstract

The objective of this paper is to design a new fuel bundle for use in a generic pressure-channel SCWR with  $UO_2$  fuel, so that the fuel channel materials, i.e., sheath and fuel, will operate below accepted temperature limits. This was achieved by modifying the flow geometry of a 43-element bundle by increasing a number of fuel elements and by decreasing their outer diameter. The proposed 64-element fuel bundle consists of 63 fuelled elements with an outer diameter of 9.1 mm, and a central element with an outer diameter of 20 mm, which is filled with the burnable poison.

### 1. Literature survey

SuperCritical Water-cooled Reactors (SCWRs) are one of the six nuclear-reactor concepts currently being developed under the Generation-IV program. Also, other Generation-IV nuclear-reactor options are: Gas-cooled Fast Reactors (GFRs), Lead-cooled Fast Reactors (LFRs), Molten Salt-cooled reactors (MSRs), Sodium-cooled Fast Reactors (SFRs), and Very High-Temperature gas-cooled Reactors (VHTRs). The main advantage of SCWRs, which use supercritical water as the reactor coolant, is an increase in the thermal efficiency from 30-34% (current level of Nuclear Power Plants (NPPs)) to 45-50% for SCW NPPs. This increase in the thermal efficiency is a result of high outlet temperature of the coolant, which can be as high as 625°C at a pressure of 25 MPa. In general, several fuel-bundle designs can be considered for Pressure-Channel (PCh) SCWRs. Some of these bundles are: 37-element, 43-element CANFLEX, 43-element Variant-18 and 43-element Variant-20, which cross sections are shown in Figures 1-4, respectively. Table 1 lists various parameters related to these four fuel-bundle designs.





Figure 1 37-element [2].





Figure 3 43-element Variant-18 [2].

Figure 4 43-element Variant-20 [2].

	<b>37-Element</b>	CANFLEX	Variant-18	Variant-20	
No. of Elements	37	43	43	43	
		Element C	DD (mm)		
Centre Ring (1 element)	13.08	13.5	18.0	20.0	
Inner Ring Elements	13.08	13.5	11.5	11.5	
Intermediate Ring Elements	13.08	11.5	11.5	11.5	
Outer Ring Elements	13.08	11.5	11.5	11.5	
Wall Thickness of Elements (mm)	0.47	0.46/0.39	-/0.39	-/0.39	
No. of Bundles Per Channel		12	2		
Heated/Total Bundle-String Length (m)		5.772/:	5.944		
Heated Area (m <sup>2</sup> )	8.76	9.26	8.76	8.76	
ID Flow Tube (mm)	103.45				
Flow Area (mm <sup>2</sup> )	3449	3625	3788	3729	
Hydraulic-equivalent Diameter: D <sub>hy</sub> (mm)	7.64	7.52	7.98	7.83	

## 2. Research

# 2.1 Reason behind designing new fuel bundles

Throughout this research project, the 43-element Variant-20 fuel bundle was used as a reference. When uranium dioxide (UO<sub>2</sub>) is used as a fuel, the fuel centerline temperature in the 43-element Variant-20 fuel bundle might exceed the industry accepted limit of  $1850^{\circ}$ C at certain conditions. Thus, either the fuel bundle has to be modified for the use of UO<sub>2</sub> fuel in SCWRs, or the use of different fuels needs to be researched.

The objective of this paper is to analyse the newly designed 64-element fuel bundle for use in a generic PCh SCWR to show that the fuel-channel materials, i.e., sheath and fuel, will operate below the accepted temperature limits.

# 2.2 The different designs

At the beginning, seven different fuel-bundle designs were proposed, each with either different outside diameters of the elements, inside diameters of the flow tubes, or number of fuel elements.

The seven cross sections below represent the fuel-bundle designs described in Table 2. The fuel bundle selected for the analysis in this paper is the 64-element fuel bundle with an outer diameter of the 42 elements 9.13 mm and the center unheated fuel -20 mm.





Figure 5 Option 1.

Figure 6 Option 2.

Figure 7 Option 3.



Figure 8 Option 4.

Figure 9 Option 5.

Figure 10 Option 6.



Figure 11 Option 7.

Table 2. Parameters	of New	Fuel	Bundles.	

	Variant- 20	Option 1	Option 2	Option 3	Option 4	Option 5	Option 6	Option 7
ID Flow	103.45	103.45	103.45	121.0	103.45	103.45	111	97.4
Tube (mm)								
OD	11.5	8.80	9.50	9.50	9.127	10.3	10.3	8.50
Elements (mm)								
OD Center	20	20	20	20	20	20	20	20
Element (mm)								
Number of	42	63	53	63	63	49	53	63
Heated								
Elements								
Total	43	64	54	64	64	50	54	64
Number of								
Elements								

Fuel-channel design for these bundles is shown in Figure 12. The operating temperature range of the coolant is from 350 to 625°C.



Figure 12 High Efficiency Fuel Channel.

# 2.3 Analysis of the 64-element fuel bundle

To be able to calculate certain parameters, some restrictions and constant values were stated. The thickness of the fuel elements were kept constant at 0.4 mm, the number of fuel bundles per bundle string was 12, the thermal power per channel was 8.5 MW, the center element was kept unheated with an outer diameter of 20 mm, and the mass flow rate was constant at 4.37 kg/s, for simplicity of the calculations. A restriction that was made on the designs was that the minimum gap between the various element pins would be no less than 1.5 mm to allow for adequate cooling of the fuel and sheath material.

	Variant	Option						
	-20	1	2	3	4	5	6	7
	ID <sub>FT</sub>							
	103.45	103.45	121.00	103.45	111.00	103.45	97.50	103.45
	mm							
	OD <sub>e</sub>							
	11.5	9.50	9.50	10.3	10.3	8.80	8.50	9.127
	mm							
				Bu	ndle			
Heated Length (m)				0.	481			
	Variant	Option						
	-20	1	2	3	4	5	6	7
Number of Elements	43	54	64	50	54	64	64	64
$V_{f}$ (cm <sup>3</sup> )	1816.57	1578.55	1876.39	1715.56	1855.60	1610.06	1502.15	1731.94

## Table 3. Main Parameters of the Seven Fuel Bundle Designs and the Variant-20.

	Variant -20	Option 1	Option 2	Option 3	Option 4	Option 5	Option 6	Option 7
$A_{h}(m^{2})$	0.73	0.76	0.90	0.76	0.82	0.84	0.81	0.87
$A_{f} (mm^2)$	3728.60	4334.34	6719.28	4008.27	4946.62	4259.36	3577.10	3969.30
D <sub>he</sub> (mm)	7.83	8.80	11.57	8.12	9.30	8.00	6.97	7.24
$P_{h}(m)$	1.52	1.58	1.88	1.59	1.71	1.74	1.68	1.81
Heated Diameter (mm)	9.83	10.96	14.29	10.11	11.54	9.78	8.51	8.79
$G (kg/m^2s)$	1172	1008	650	1090	883	1026	1222	1101
				Bundl	e String			
Heated Length (m)				:	5.772			
$A_{h}(m^{2})$	8.76	9.13	10.85	9.15	9.90	10.05	9.71	10.43
$q (kW/m^2)$	970.5	931.0	783.2	928.8	858.7	845.5	875.4	815.2
$V_{f}$ (dm <sup>3</sup> )	21.8	18.9	22.5	20.6	22.3	19.3	18.0	20.8

\* FT: Flow Tube

A three-dimensional model was created of the 64-element fuel bundle using UGS NX 7.5 Software. Three programs were created through Matlab to further analyse the fuel bundle. The first program created used advanced geometry to draw a fuel bundle to the specifications of the user. The program is then linked to two other programs that calculates thermalhydraulic variables according to the bundle modelled in the first program.

To calculate the heat transfer coefficient, the Mokry et al. equation was used:

$$HTC(i) = \frac{k_{bulk}(i)}{1000 \cdot D_{hy}} \cdot 0.0061 \cdot \left(\frac{G \cdot D_{hy}}{\mu_{bulk}(i)}\right)^{0.904} \Pr_{avg}(i)^{0.684} \cdot \left(\frac{\rho_{wall}(i)}{\rho_{bulk}(i)}\right)^{0.564}$$
(1)
$$\Pr_{avg}(i) = \frac{Cp_{avg}(i) \cdot \mu_{bulk}(i)}{k_{bulk}(i)}$$
(2)

As can be seen in Figures 14 and 15, under some conditions the fuel centerline temperature for the reference 43-element Variant-20 fuel bundle with  $UO_2$  as a fuel may exceed the industry accepted limit of 1850°C. However, the fuel centerline temperature in Figure 16 is approximately 1400°C, i.e., 450°C below that of the industry accepted limit. The fuel center line temperature in Figure 17 is approximately 1500°C, i.e., 350°C below that of the industry accepted limit.



Figure 13 Axial Heat Flux Profiles (AHFPs).



Figure 14 Cosine AHFP, UO<sub>2</sub> fuel, Variant-20 bundle.



Figure 15 Down-stream Skewed AHFP, UO<sub>2</sub> fuel, Variant-20 bundle.



Figure 16 Cosine AHFP, UO<sub>2</sub> fuel, 64-element bundle.



Figure 17 Down-stream Skewed AHFP, UO<sub>2</sub> fuel, 64element bundle.

#### 3.0 Conclusion

A new 64-element fuel bundle was designed to operate at supercritical-water conditions with an outlet temperature of  $625^{\circ}$ C at 25 MPa as a replacement for the 43-element Variant-20 fuel bundle, which might not be used at these conditions in application to SCWR, because within certain conditions, such as cosine and downstream-skewed cosine AHFPs, the fuel centerline temperature may exceed the industry accepted limit of  $1850^{\circ}$ C when UO<sub>2</sub> is utilized as a fuel. The fuel centerline temperatures in the 64-element bundle with smaller OD fuel elements are below the industry accepted limit by 450 and 350°C at cosine and downstream-skewed cosine AHFPs, respectively. These results show that the 64-element fuel bundle can be a potential candidate for implementation in SCWRs.

4.0	Nomenclature	$ID_{PT}$ :	Inner Diameter of the
			Perforated Tube
$V_f$ :	Fuel Volume	$D_{he}$ :	Hydraulic-Equivalent
$ID_e$ :	Inner Diameter of the		Diameter
	Elements	$P_w$ :	Wetted Perimeter
$N_h$ :	Number of Heated Elements	$P_h$ :	Heated Perimeter
$A_h$ :	Heated Area	G:	Mass Flux
$OD_e$ :	Outer Diameter of the	ṁ:	Mass Flow Rate
	Elements	q:	Heat Flux
$A_f$ :	Flow Area	HTC:	Heat Transfer Coefficient

k <sub>bulk</sub> :	Thermal Conductivity	AHFP:	Axial Heat Flux Profile
$D_{hy}$ :	Hydraulic Diameter	$UO_2$ :	Uranium Dioxide
$\mu_{bulk}$ :	Dynamic Viscosity	GFRs:	Gas Cooled Fast Reactors
$\rho_{wall}$ :	Wall Density	LFRs:	Lead-Cooled Fast Reactors
$\rho_{bulk}$ :	Bulk Density	MSRs:	Molten Salt-Cooled Reactors
Pravg:	Average Prandtl Number	SFRs:	Sodium Cooled Fast Reactors
$Cp_{avg}$ :	Average Specific Heat	VHTRs:	Very High-Temperature Gas-
- 0			Cooled
			Reactors
5.0	Abbreviations and Acronyms	CANDU:	Canada Deuterium Uranium
		REFPROP:	<b>REFerence PROPerties</b>
SCWR:	SuperCritical Water-cooled	MATLAB:	MATrix LABoratory
	Reactor	CANFLEX:	CANdu FLEXible Fuelling

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