STATUS OF VALIDATION MATRICES FOR CANDU[®] POWER PLANTS

by

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ABSTRACT

As reported at the 1996 CNS Annual Conference, in mid-1995 the CANDU[®] industry began to develop validation matrices for CANDU power plants. Of the eight matrices required to address all physical phenomena that could occur in all relevant accident categories, two have been prepared and tabled with the Atomic Energy Control Board, and the remaining six are targeted for submission during 1997. The matrices provide the generic, codeindependent knowledge base that will be used to validate major safety analysis codes over the next four years. The unique achievement reported in this paper is the identification and listing of all physical phenomena in all relevant accident categories.

1. INTRODUCTION

Computer codes for the analysis of accidents in CANDU power plants have been in use since the 1960s. With time, many of these codes have been revised and improved and some new ones have been written, to capture greater detail and/or new information from research laboratories and operating plants. To meet today's quality assurance standards, such codes, often referred to as 'scientific computer codes', must be qualified and used according to defined procedures.

Qualification of Scientific Computer Codes

The Canadian approach to code qualification covers several elements in a broadly based, integrated approach. The main elements include:

- a review of codes in current use, to target those that are to be used for the long term;
- a review and identification of safety analysis function needs, including future needs;
- the development of code migration plans to arrive, as far as possible, at a set of industry standard tools for safety analysis;

and for the targeted codes.

- an assessment of their current level of qualification,
- development of verification and validation plans for their further qualification,

- execution of verification plans,
- · development of a knowledge base (validation matrices) for their systematic validation,
- execution of validation plans, and
- documentation of the verification and validation work.
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This paper provides an update on the development of the knowledge base and briefly mentions some of the code validation plans. The other elements are being addressed separately by the individual organizations, although the Industry Standard Toolset initiative, currently under way, provides an opportunity to join forces on some elements. The industry's target date for completion of the validation program is late 2000/early 2001.

Validation Matrices

The validation aspect can be considered in two phases: the generic, i.e. knowledge-based, code independent component, and a code-specific component. The Nuclear Energy Agency (NEA) of the Organization for Economic Co-operation and Development (OECD) developed a methodology for addressing the generic component for Light Water Reactors^[1]. It is based on a 'validation matrix' that has two tables. The first identifies physical phenomena that could occur in the specified accident categories. The second identifies data sets that exhibit the physical phenomena and could be used to validate specific codes. The OECD/NEA produced a validation matrix for system thermalhydraulics of pressurized water and boiling water reactors^[1], and it is currently working on a State-of-the Art-Report (SOAR) on Containment Thermalhydraulics and Hydrogen Distribution^[2], which is proposed to include a sample matrix for containment behaviour phenomena under a PWR severe accident scenario. AECL is an active participant in the development of the SOAR, as the lead author for a main chapter on Recent Experimental Activities (Chapter 4).

In mid-1995, the Canadian CANDU industry, comprising Atomic Energy of Canada Limited (AECL), Hydro Quebec (HQ), Ontario Hydro Nuclear (OHN), and New Brunswick Power (NBP), decided to adopt the principles of the validation-matrix methodology and adapt them to CANDU power plants, to address all aspects of its safety analysis, not just system thermalhydraulics and containment. In particular, the industry chose eight scientific disciplines to cover the entire safety analysis:

- (i) System Thermalhydraulics;
- (ii) Fuel and Fuel Channel Thermal-mechanical Behaviour;
- (iii) Fission Product Release and Transport;
- (iv) Containment Behaviour;
- (v) Reactor Physics;
- (vi) Radiation Physics,
- (vii) Atmospheric Dispersion; and
- (viii) Moderator and Shield System Thermalhydraulics.

To manage and perform the work, the Canadian CANDU industry decided to create an Industry Validation Team. The Team comprises a Steering Group of eight senior managers, to co-ordinate the overall effort, and 11 Working Groups and a sub-group, currently of ~90 specialists and technical managers, to develop the validation matrices, develop a technical basis, address uncertainties in code predictions, and develop the knowledge base for small reactors. The lead Working Group, on System Thermalhydraulics, has developed its validation matrix, which was the example used in the 1996 CNS paper on the industry-wide validation effort^[3]. Since then, the Working Group on Fuel and Fuel Channel Thermal-mechanical Behaviour has also produced its validation matrix. The other Working Groups have developed, as a minimum, their lists of accident categories and physical phenomena, covering all aspects of CANDU safety analysis. To the authors' knowledge, this is a unique achievement for any nuclear reactor. The lists are the principal subject of this paper, and progress is reported on the identification of data sets and documentation of all aspects of generic validation. Future plans in this multi-year, industry-wide code qualification program are also addressed briefly.

^{*} In the 1996 CNS paper^[3], Reactor Physics, Radiation Physics, and Atmospheric Dispersion were shown as Subgroups of Physics. In reality, specialists in these three areas have been working autonomously.

Definition of Phenomenon

Webster defines a phenomenon as - Any event, circumstance, or experience that is apparent to the senses and that can be scientifically described or appraised. This definition is difficult to apply in the present context, and therefore the following working definition was used^[4].

- A phenomenon is an event or circumstance that:
 - a) characterizes the process of changing the physical state of a system, and
 - b) is either directly apparent to the senses or is indirectly apparent by means of measurements of the physical state of a system.

With this definition as a "filter", all phenomena relevant to the eight scientific disciplines were compiled. The definition was followed rigorously, to prevent confusion with properties, mechanisms, behaviours, mathematical correlations, effects, etc. Thus, for example, drift flux in two-phase flow is a mathematical representation of different phase velocities, not a physical phenomenon. Phase separation is the appropriate phenomenon for this example.

The relevant accident categories and physical phenomena are presented in Lists 1 to 17.

2. TECHNICAL BASIS DOCUMENT

The Technical Basis Document provides the overall 'road map' to the validation-matrix methodology. It identifies the accident categories, and for each accident category, the safety concerns, behaviours of systems and radionuclides, and main physical phenomena, as described in more detail in Reference 3. The Technical Basis Document is being written, and its target completion date is the end of 1997. The table of contents has been drafted and is shown in the Attachment. Section 1, the large loss-of-coolant accident (LOCA), has been documented and reviewed^[5], and it is being used as a model for the production of the remaining sections. A lengthy excerpt from section 1 is shown in the Attachment, to illustrate the descriptive style adopted for this document.

3. SYSTEM THERMALHYDRAULICS

The validation matrix in System Thermalhydraulics was on hand in 1995 December and was used to illustrate the methodology adopted for the industry-wide validation work^[3]. For completeness, Lists 1 and 2 are presented here, showing the relevant accident categories and the physical phenomena, respectively^[4]. The next steps in the validation methodology, namely code-specific validation plans, validation exercises, and validation manuals, are currently being developed and executed for the two-fluid systems codes CATHENA and TUF. The former is being used by AECL, HQ, and NBP, and the latter by OHN. This part of the code qualification program is tentatively scheduled for completion by late 2000/early 2001.

4. FUEL AND FUEL CHANNEL THERMAL-MECHANICAL BEHAVIOUR

The Working Group on Fuel and Fuel Channel Thermal-mechanical Behaviour has submitted revision 0 of its validation-matrix report to the Atomic Energy Control Board in 1996 December. The report identifies 23 physical phenomena that could occur in eight accident categories, Lists 4 and 3. The phenomena are ranked for one of them, the large LOCA. The data sets include: 19 accidents in reactors, one analytical solution, 5 cross-code comparisons, 33 out-reactor integrated tests, 49 in-reactor tests, and 55 separate-effects tests. All phenomena synopses and most of the data set synopses have been produced, and drafting of the remaining ones is under way.

4.1 Fuel Channel Thermalhydraulics

A Sub-group on Fuel Channel Thermalhydraulics has identified 20 physical phenomena in seven accident categories, Lists 17 and 16, and produced short descriptions of the phenomena. The Sub-group has updated its phenomenon/ accident table, draft ranked the phenomena, and preliminarily identified relevant experiments. The work of the Subgroup is being reformatted so that it can be integrated with future revisions of the validation matrices in System Thermalhydraulics and in Fuel and Fuel Channel Thermal-mechanical Behaviour.

5. FISSION PRODUCT RELEASE AND TRANSPORT

The Working Group on Fission Product Release and Transport has identified 19 physical phenomena in the subdiscipline of fission product release and 23 in fission product transport, List 6, and produced synopses of all of them. The relevant accident categories are shown in List 5. The Working Group has also identified 120 data sets and produced synopses of them. Their validation-matrix report is in the final stage of industry review and approval. This Working Group was the first to adopt the Microsoft relational data base ACCESS for their work and used it to great advantage in the course of their peer review and resolution of comments. They are now also in an excellent position to automatically manage revisions to, and control the configuration of their validation matrix. In addition to facilitating review and production of the 1200 page document, the ACCESS data base proved to be very space efficient in terms of storage. The single-file data base is less than three megabytes in size, and following compression, will fit on a single '3.5 inch' floppy diskette. Since the Industry Validation Team decided in 1997 April to eventually convert all matrices to ACCESS format, automatic conversion macros are being developed in MS Word 6.0. In addition, support of tables, figures, and other graphics is being actively explored.

The contributions from the Working Group to the Technical Basis Document are being drafted and reviewed, with a target completion date of mid-1997.

6. CONTAINMENT BEHAVIOUR

The Working Group on Containment Behaviour has identified 10 physical phenomena in the sub-discipline of containment thermalhydraulics, nine in hydrogen behaviour, seven in iodine chemistry, and 16 in aerosol behaviour, List 8. Combinations of these phenomena could occur in seven accident categories, List 7. Because of the multi-disciplinary nature of containment analysis, the list is divided into four sub-disciplines that have traditionally used different analysis codes. These sub-disciplines are Thermalhydraulics, Hydrogen Behavior, Iodine Chemistry, and Aerosol Behavior. Fission products other than iodine appear as aerosols in containment and are treated under the aerosol behavior sub-discipline. The Working Group has also identified seven numerical/analytical tests, 25 separate effects tests, and 17 integrated effects tests. The experimental database available for use in the validation of CANDU containment codes encompasses experiments and test facilities from around the world. Some of the tests were designed to be CANDU specific, while most are used worldwide for generic containment code validation. Synopses of phenomena and data sets and the contribution to the Technical Basis Document are being drafted. The target date for the completion of revision 0 of the validation-matrix report is mid-1997.

7. REACTOR PHYSICS

The Working Group on Reactor Physics has identified 16 physical phenomena that could occur in 15 accident categories, Lists 10 and 9. All phenomena synopses have been written and reviewed, and synopses of data sets from experiments in research reactors (primarily ZED-2 and NRU at the Chalk River Laboratories) and commissioning tests in Canadian CANDU reactors have been drafted. The Working Group was the second to adopt ACCESS for the production and configuration management of its validation-matrix report, which has been assembled and sent for industry review. The target date for its submission to the AECB is mid-1997.

8. RADIATION PHYSICS

The Working Group on Radiation Physics has identified 10 physical phenomena in five accident categories, Lists 12 and 11, and is currently drafting synopses of the phenomena. The target date for the completion of revision 0 of the validation-matrix report is the end of 1997.

9. ATMOSPHERIC DISPERSION

The Working Group on Atmospheric Dispersion has identified 15 physical phenomena, List 13, that need to be considered in the calculation of radiation doses to humans exposed to radioactive emissions, and has drafted synopses of the phenomena. Many phenomena related to atmospheric dispersion are independent of the accident that led to the release. The relative importance of other phenomena has been found to be more closely related to containment response rather than accident type. Containment response is itself dependent on the containment design concept, for example, whether a negative-pressure or positive-pressure design is employed. The final form of the atmospheric dispersion matrix is expected to reflect these considerations. The target date for the completion of revision 0 of the validation-matrix report is the end of 1997.

10. MODERATOR AND SHIELD SYSTEM THERMALHYDRAULICS

The Working Group on Moderator and Shield System Thermalhydraulics has identified 19 physical phenomena that could occur in 15 accident categories, Lists 15 and 14, and has drafted all phenomena synopses. The Working Group has also produced flow charts of safety concerns, behaviours, and phenomena that will be useful in the preparation of their contribution to the Technical Basis Document. They are presently preparing data set synopses. The target date for the completion of revision 0 of the validation-matrix report is the end of 1997.

11. SMALL REACTORS

While the main focus of the Industry Validation Team is the generic validation of computer codes for CANDU analyses, the Team also has a Working Group on Small Reactors which is developing a Technical Basis Document and validation matrices for pool reactors, principally those of the MAPLE family. Typically, the documents being produced by that Working Group are addenda to the documents arising from the work of their CANDU colleagues.

12. UNCERTAINTY ANALYSIS

A Working Group on Uncertainties in Code Predictions is developing practical methodologies that promise to be broadly applicable to the estimation of uncertainties in key outputs from safety analysis codes. Because of its exploratory nature, that work has not been planned in detail as yet and is expected to continue several years into the future.

13. LESSONS LEARNED

The Industry Validation Team first met in mid-1995 as a small group of senior managers from AECL, HQ, OHN, and NBP, with a common interest: to address systematic validation of major computer codes used in safety analyses of CANDU power plants. The group quickly realized that a large, industry-wide effort was required and that flexible collaboration arrangements were desirable, to maximize productive deployment of scare resources. The number of partcipants in the activity grew to ~100, most of whom are senior specialists and technical managers in their respective disciplines and some of whom have been assigned full time to this work. As the work progressed, some working protocols were adopted, and decisions were made, usually by consensus, to achieve as high a degree of uniformity as possible in the end products, i.e., the validation matrices. Some of the main lessons learned from the effort to date are itemized briefly below.

Organizational Aspects

• The Industry Validation Team adopted Terms of Reference and Working Protocols, to define roles and working relationships among the Steering Group, Working Groups, line managers in the participating organizations, and

the regulator, i.e., the Atomic Energy Control Board, for communications, interactions, and reporting requirements. Working Groups were given a large degree of autonomy in defining their mode of operation, choosing their members, assigning responsibilities to their members, etc. Generic validation-matrix reports were seen as the end product of the industry-wide effort, and once these were on hand, the Industry Validation Team would have fulfilled its mandate. Subsequent validation of individual computer codes was seen as the responsibility of each participating organization. This flexible organizational structure and work by consensus have been, and continue to be highly effective in developing validation matrices in parallel on a short schedule.

- It was agreed that the Industry Validation Team would have no official status vis-a-vis the regulator, but would
 provide information and be available for informal discussions. Formal commitments and official submissions
 would continue to be the prerogative of the participating organizations, via existing communication channels.
- As the generic validation work is approaching completion, executive line management of the industry has recognized that the Industry Validation Team has become a valuable resource and should not disband, once it has completed its generic validation matrices. The Team is in the best position to provide continued leadership on validation activities. Thus, the Steering Group has been given the mandate to lead the process of selecting an Industry Standard Toolset, for safety analyses of CANDU power plants. The intent is to choose appropriate computer codes for use by the industry and to focus further development effort on them, including validation. To date, five Working Groups under the Industry Standard Toolset initiative have been formed and charged with examining in detail specific computer codes in their respective disciplines, with a view of recommending standard sets. Some successes have been achieved already, and prospects are good for consensus on additional codes. However, it is likely that several separate codes will remain in use in the industry.

Validation-Matrix Completeness and Interfaces

- As the Working Groups identified their respective lists of accident categories, physical phenomena, and data sets, it became important to ensure completeness, avoid duplication of effort, and use common definitions. One senior analyst was given the responsibility of collecting these draft lists, reviewing them, and assigning responsibility to a lead Working Group for the definition of each phenomenon that was common to one or more Working Groups. The Working Groups themselves were charged with reviewing draft lists and synopses of 'adjacent' Groups, to ensure consistency in the usage of overlapping accident categories, phenomena, and data sets. The Working Group on the Technical Basis Document was assigned overall responsibility for co-ordinating inputs from the other Working Groups into that document. The success to date of these interactions is apparent from the completed lists of accident categories and phenomena given in Lists 1 to 17. Detailed phenomena and data set synopses, too voluminous to be reproduced here, provide specific cross-links within and among the validation matrices.
- Development of validation-matrices was, and continues to be a learning experience for all participants. As in any first-of-its-kind endeavour, the developers and reviewers, including AECB staff, identified improvements that could be made. Rather than expending resources on successive iterations and improvements, the Industry Validation Team decided to complete the entire validation cycle. Thus, upon completion of the initial validation matrix in each discipline, effort and priority was, and is given to producing code specific validation plans, exercises, and validation manuals.

Configuration Management

Each validation-matrix report captures a large volume of information that is written, assembled, and reviewed by many specialists over a period of time of a year or two. Such an endeavour naturally raises issues of resolution of comments, version control, and overall configuration management. The lead Working Groups managed these issues as they arose and produced revision 0 (and in one instance revision 1) reports. The Working Group on Fission Product Release and Transport spearheaded a radically different approach. Part way into its validation-matrix development work, the Group decided to adopt the Microsoft relational data base ACCESS, to convert the existing records into it, and to complete the remaining work in ACCESS. This decision turned out to be a resounding success. The Group executed the conversion in a very short time and reaped downstream benefits during the review and record keeping stages. ACCESS lends itself naturally to auditable resolution of comments, version control, and configuration management. Individual records and linkages among them are entered once, and

thereafter the data base keeps track of them. A custodian keeps the master version and controls revisions. All these features should make it easier for the regulator to review the validation-matrix document.

On the basis of the excellent experience described above, the Industry Validation Team decided to convert all validation-matrix reports to ACCESS, with the timing of that conversion left to the Working Groups.

• As part of the process of generating the validation matrices, unique identifiers have been assigned to phenomena and data. In some instances, as the work progressed, it became apparent that some phenomena or data needed to be removed. Instead of changing the identifiers on all subsequent phenomena or data and searching for cross-references in the entire set of documents to make corrections, it was decided to leave gaps in the sequence of identifiers. Thus, for example, in List 12, there is no phenomenon RAD10. At some future point, when all validation matrices are in the ACCESS data base, it would be relatively easy to re-number phenomena and data to remove gaps.

Data Sets

- The issue of qualification of data sets shown in validation matrices was resolved as follows. The matrix developers need to satisfy themselves, via inspection of the data and a preliminatry qualification of them, that they may be suitable for code validation. A more detailed qualification of data selected for the validation of a specific computer code is to be performed for the code validation plan.
- During the search for data sets, some Working Groups have identified data that are known to exist but are not
 readily available to the Group, mainly because they are owned by other organizations. It was agreed that such data
 sets would not be shown in the validation matrices, although their existence would be acknowledged in working
 documents, such as minutes of meetings, to provide a trail to show that the Working Group was aware of the data.
 If such data are 'more of the same', i.e. do not add significantly to the available data sets, then their omission is no
 great loss. If such data are unique or the only existing experimental information, then the Steering Group decides
 on the most appropriate way of addressing them.
- In some data searches, data have been identified that are. or could become unavailable because of neglect, i.e. because they are about to be abandoned or otherwise destroyed. Typically, such data are old, difficult to access with today's electronic technology, and would require an investment of expert staff time to make them readily available. Working Parties of the CANDU Owners Group (COG) already have a mandate and action to identify such data and to preserve them.
- Some data sets have been identified that are not directly applicable to the phenomena of interest, for example because they lie outside the range of CANDU analyses. The Industry Validation Team decided that, if data within the range are available, then there is no need to include data outside the range. If not, then data outside the range should be included, provided that they exhibit the phenomena of interest. The phenomenon description is to address this issue under 'State of Knowledge and Uncertainties'. A given code should be validated with best available data, even when outside the range of interest.
- Overlapping data sets present no problem and are shown in the validation matrices. During the code-specific validation stage, data are selected and that selection is described in the code validation plan.
- When Working Groups identify data gaps in validation matrices, they use the COG process to set priorities for new work, call for proposals, and invite R&D proponents to respond.

14. SUMMARY AND CONCLUSIONS

In summary, the Industry Validation Team is on track in its program to develop a generic knowledge foundation, based on validation matrices, for the validation of computer codes used in safety analyses of CANDU plants. The Team has ~100 participants from the Canadian CANDU industry, comprising Atomic Energy of Canada Limited, Hydro Quebec, Ontario Hydro Nuclear, and New Brunswick Power, organized into a Steering Group of eight senior managers and 11 Working Groups and a Sub-group of technical specialists and technical managers. Two of eight validation matrices have been submitted already to the regulator, the Atomic Energy Control Board, and the remaining six are targeted for completion during 1997. The 'road map' for the validation matrices, i.e., a single Technical Basis Document, is also being drafted and targeted for completion before the end of 1997. Based on this generic foundation, code-specific validation plans are being developed and executed by the individual industry organizations, with a target completion date of late 2000/early 2001.

Code validation is one element of a broadly based, integrated program of code qualification undertaken by the individual industry organizations and targeted for completion by late 2000/early 2001.

15. ACKNOWLEDGMENT

The authors have assumed the role of Rapporteur for work done by others, namely, the ~90 specialists and technical managers throughout Atomic Energy of Canada Limited, Ontario Hydro Nuclear, Hydro Quebec, and New Bruswick Power who have, and are developing the validation matrices with great dedication and enthusiasm. Their efforts are hereby acknowledged.

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List 1: Accident Categories Relevant to CANDU System Thermalhydraulics

Large LOCA Power Pulse/Reactor Trip Early Blowdown Cooling Late Blowdown Cooling/Emergency Coolant Injection Refill Large LOCA/LOECI Power Pulse/Reactor Trip Early Blowdown Cooling Steam Cooling/Heat Rejection To Moderator Small LOCA Depressurization Reactor Trip ECI Refill Loss of Flow Loss of Class IV Power - Pump Rundown Two-Phase Thermosiphoning Intermittent-Boiling-Induced Flow Loss of Regulation Power Increase/Reactor Trip Fuel Channel Quench Loss of Feedwater PHTS Pressurization/Reactor Trip Long Term Cooling Steam Line Breaks Steam Generator Blowdown Reactor Trip Loss of Class IV Power ECI

List 2: Physical Phenomena Relevant to CANDU System Thermalhydraulics

ID Phenomenon

- TH1 Break Discharge Characteristics and Critical Flow
- TH2 Coolant Voiding
- TH3 Phase Separation
- TH4 Level Swell and Void Holdup
- TH5 Heat-Transport Pump Characteristics (Single-and Two-Phase)
- TH6 Thermal Conduction
- TH7 Convective Heat Transfer
- TH8 Nucleate Boiling Heat Transfer
- TH9 CHF and Post-Dryout Heat Transfer
- TH10 Condensation Heat Transfer
- TH11 Radiative Heat Transfer
- TH12 Quench/Rewet Characteristics
- TH13 Zirconium/Water Thermal-Chemical Reaction
- TH14 Reflux Condensation
- TH15 Counter-Current Flow
- TH16 Flow Oscillations
- TH17 Density Driven Flows: Natural Circulation
- TH18 Fuel Channel Deformation
- TH19 Fuel String Mechanical-Hydraulic Interaction
- TH20 Waterhammer
- TH21 Waterhammer: Steam Condensation Induced
- TH22 Pipe Thrust and Jet Impingement
- TH23 Non-Condensable Gas Effect
- List 3: Accident Categories Relevant to CANDU Fuel and Fuel Channel Thermalmechanical Behaviour

Large LOCA

Loss of Flow

Loss of Regulation

Large LOCA/LOECI Small LOCA End fitting failure Stagnation Feeder Break Flow Blockage Fuel Handling Accidents

List 4: Physical Phenomena Relevant to CANDU Fuel and Fuel Channel Thermalmechanical Behaviour

ID Phenomenon

- FC1 Fission and Decay Heating
- FC2 Heat Diffusivity in Fuel
- FC3 Fuel-to-Sheath Heat Transfer
- FC4 Fuel-to-End-Cap Heat Transfer
- FC5 Fission Gas Release to Gap and Pressurization
- FC6 Sheath Deformation
- FC7 Sheath Failure
- FC8 Fuel Deformation
- FC9 Sheath Oxidation/Hydriding
- FC10 Fuel Oxidation/Reduction
- FC11 Fuel, Sheath Melting and Relocation
- FC12 Bundle Mechanical Deformation
- FC13 Sheath-to-Coolant and Coolant-to-Pressure Tube Heat Transfer
- FC14 Flow Mixing and Bypass
- FC15 Local Melt Heat Transfer to Pressure Tube
- FC16 Pressure Tube to Calandria Tube Heat Transfer
- FC17 Calandria Tube to Moderator Heat Transfer
- FC18 Pressure Tube Deformation and Failure
- FC19 Calandria Tube Deformation and Failure
- FC20 Pressure Tube Oxidation and Hydriding
- FC21 Element/Pressure Tube Radiative Heat
- FC22 Element/Bearing Pad/Pressure Tube Contact Heat Transfer
- FC23 Failed Channel Interaction With Core Components

List 5: Accident Categories Relevant to CANDU Fission Product Release and Transport

Large LOCA

Small LOCA End Fitting Failure Stagnation Feeder Break Flow Blockage Large LOCA/LOECI Secondary Side Breaks Fuel Handling Accidents

- List 6: Physical Phenomena Relevant to CANDU Fission Product Release and Transport
- ID Phenomenon

Fission Product Release

FPR-1 Athermal Release FPR-2 Diffusion FPR-3 Grain Boundary Sweeping/Grain Growth FPR-4 Grain Boundary Coalescence/Tunnel Interlinkage FPR-5 Vapor Transport/Columnar Grains FPR-6 Fuel Cracking (Thermal) FPR-7 Gap Transport (Failed Elements) FPR-8 Gap Retention FPR-9 UO2+x Formation FPR-10 U4O9 - U3O8 Formation FPR-11 UO_{2-x} Formation FPR-12 UO₂ Zircaloy Interaction FPR-13 UO₂ Dissolution by Molten Zircaloy FPR-14 Fuel Melting FPR-15 Fission Product Vaporization/Volatilization FPR-16 Matrix Stripping FPR-17 Temperature Transients FPR-18 Grain Boundary Separation FPR-19 Fission Product Leaching **Fission Product Transport** FPT-1 Fuel Particulate Suspension FPT-2 Vapour Deposition and Re-vaporization of Deposits FPT-3 Vapour/Structure Interaction FPT-4 Aerosol Nucleation FPT-5 Gravitational Agglomeration in the Primary Heat Transport System (PHTS) FPT-6 Brownian Motion (Diffusional) Agglomeration in PHTS FPT-7 Turbulent Agglomeration in PHTS FPT-8 Laminar Agglomeration FPT-9 Electrostatic Agglomeration FPT-10 Aerosol Growth/Revapourization FPT-11 Thermophoretic Deposition in PHTS FPT-12 Diffusiophoretic Deposition FPT-13 Gravitational Deposition FPT-14 Brownian Motion Deposition FPT-15 Turbulent Deposition in PHTS FPT-16 Laminar Deposition FPT-17 Electrostatic Deposition FPT-18 Inertial Deposition FPT-19 Photophoretic Deposition FPT-20 Aerosol Resuspension FPT-21 Pool Scrubbing FPT-22 Transport of Deposits by Water FPT-23 Chemical Speciation FPT-24 Transport of Structural Materials

List 7: Accident Categories Relevant to CANDU Containment Behaviour

Large LOCA Small LOCA Pipe Breaks In-Core Breaks Large LOCA/LOECI Secondary Side Breaks Fuel Handling Accidents Auxiliary System Failures

List 8: Physical Phenomena Relevant to CANDU Containment Behaviour

ID Phenomenon

Thermalhydraulics

- C1 Flashing Discharge
- C2 Evaporation from Pools
- C3 Convection Heat Transfer
- C4 Conduction Heat Transfer
- C5 Condensation Heat Transfer
- C6 Air Cooler Heat Transfer
- C7 Heat Removal by Dousing Water
- C8 Laminar/Turbulent Leakage Flow
- C9 Choked Flow through Pressure Reducing Valves
- C10 Liquid Re-entrainment Hydrogen Behaviour
- C11 Buoyancy Induced Mixing
- C12 Jet Momentum Induced Mixing
- C13 Hydrogen Stratification
- C14 Hydrogen Deflagration
- C15 Flame Acceleration
- C16 Flame Quenching by Turbulence
- C17 Standing Flame
- C18 Deflagration Detonation Transition
- C19 Mixing and Removal by Recombiners Iodine Chemistry
- C21 Interfacial Mass Transfer
- C22 Partition Coefficient
- C23 Adsorption
- C24 Carbon Filter Removal Efficiency
- C25 Total Waterborne Iodine
- C26 Fraction Airborne Organic Iodine
- C27 Total Airborne Iodine

Aerosol Behaviour

- C28 Jet Impingement
- C29 Plateout (Gravitational Settling)
- C30 Thermophoresis
- C31 Diffusiophoresis
- C32 Diffusional Agglomeration
- C33 Removal in HEPA Filters
- C34 Removal in Demisters
- C35 Removal in Leakage Paths
- C36 Condensation
- C37 Evaporation
- C38 Turbulent Agglomeration

- C39 Turbulent Deposition
- C40 Formation in a Flashing Jet
- C41 Formation in a Steam Jet
- C42 Gravitational Agglomeration
- C43 Inertial Deposition

List 9: Accident Categories Relevant to CANDU Reactor Physics

Large LOCA

Emergency Coolant Injection and Class IV Power Intact Loss of Emergency Coolant Injection Loss of Class IV Power **Transition Break LOCA** Small Out-of-Core LOCA **Small In-Core LOCA** Pressure Tube/Calandria Tube Failure Stagnation Feeder Break **End-Fitting Failure** Loss of Flow Loss of Regulation Slow Fast Loss of Feedwater **Steam Line Break** Moderator System Loss of Moderator Inventory Loss of Moderator Heat Sink

List 10: Physical Phenomena Relevant to CANDU Reactor Physics

ID Phenomenon

- PH1 Coolant-Density-Change Induced Reactivity
- PH2 Coolant-Temperature-Change Induced Reactivity
- PH3 Moderator-Density-Change Induced Reactivity
- PH4 Moderator-Temperature-Change Induced Reactivity
- PH5 Moderator-Poison-Concentration-Change Induced Reactivity
- PH6 Moderator-Purity-Change Induced Reactivity
- PH7 Fuel-Temperature-Change Induced Reactivity
- PH8 Fuel-Isotopic-Composition-Change Induced Reactivity
- PH9 Refuelling-Induced Reactivity
- PH10 Fuel-String-Relocation Induced Reactivity
- PH11 Device-Movement Induced Reactivity
- PH12 Prompt/Delayed Neutron Kinetics
- PH13 Flux-Detector Response
- PH14 Flux And Power Distribution (Prompt/Decay Heat) in Space and Time

PH15 Lattice-Geometry Reactivity Effects

PH16 Coolant-Purity-Change Induced Reactivity

List 11: Accident CategoriesRelevant to CANDU Radiation Physics

Large LOCA Fuel Channel Decay Heat Moderator Heat Load Containment Activity Monitor Small LOCA End Fitting Failure Nuclear Criticality Inadvertent Nuclear Excursion

List 12: Physical Phenomena Relevant to CANDU Radiation Physics

ID Phenomenon

- RAD1 Radiation Emission
- RAD2 Isotope Generation and Depletion
- RAD3 Neutron Transport and Streaming
- RAD4 Photon Transport, Streaming and Skyshine
- RAD5 Electron Transport
- RAD6 Heating
- RAD7 Internal and External Exposure
- RAD8 Radiolysis
- RAD9 Damage
- RAD11 Criticality and Sub-Critical Multiplication

List 13: Physical Phenomena Relevant to Atmospheric Dispersion from CANDU Plants

ID Phenomenon

- AD-01 Plume Rise
- AD-03 Downwash
- AD-04 Modification of Effective Release Height Due to Building Entrainment
- AD-05 Plume Broadening Due to Building Entrainment
- AD-06 Fumigation
- AD-07 Formation of the Thermal Internal Boundary Layer
- AD-08 Reflection from an Elevated Inversion
- AD-09 Plume Advection
- AD-10 Plume Diffusion
- AD-11 Wet Deposition
- AD-12 Dry Deposition
- AD-13 Plume Depletion
- AD-14 Exposure to Cloudshine

- AD-15 Exposure to Groundshine
- AD-16 Internal Exposure due to Inhalation
- List 14: Accident Categories Relevant to CANDU Moderator and Shield System Thermalhydraulics

Loss of Moderator Heat Sink Loss of Moderator Inventory Loss of Moderator Temperature Control Low Loss of Shield Tank/End Shield Inventory Loss of Shield Tank Temperature Control Low Loss of Shield Cooling Small LOCA In-Core Breaks In-Core Breaks from a Guaranteed Shutdown State Out-of-Core Breaks Small LOCA/LOECI In-Core Breaks Large LOCA Large LOCA/LOECI Secondary Side Breaks Loss of Flow Loss of Regulation

List 15: Physical Phenomena Relevant to CANDU Moderator and Shield System Thermalhydraulics

ID Phenomenon

- MH3 Moderator Degassing
- MH4 Mass and Energy Transfer in Moderator Cover Gas
- MH9 Moderator Pump Cavitation
- MH10 Interaction of Moderator Flow with Calandria Tubes
- MH11 Moderator Flow Turbulence
- MH12 Moderator Buoyancy
- MH13 Moderator Inlet Jet Development
- MH15 Displacement of Poison from Containers
- MH16 Injection of Poison along Nozzles
- MH19 Moderator/Coolant/Poison Mixing
- MH22 Calandria Tube/Moderator Heat Transfer
- MH30 Failed Channel Interaction with Core Components
- MH34 Hydrogen Deflagration
- MH39 Moderator Heat Exchanger Response
- MH41 Liquid, Vapor and Two-Phase Discharge
- MH42 Moderator Swell
- MH43 Thermal Conduction
- MH44 Convective Heat Transfer
- MH45 Radiative Heat Transfer

List 16: Accident Categories Relevant to CANDU Fuel Channel Thermalhydraulics

Large LOCA Large LOCA/LOECI Small LOCA Pressure Tube Failure, Calandria Tube Intact In-Core Breaks Out-of-Core Breaks Loss of Flow Loss of Regulation

List 17: Physical Phenomena Relevant to CANDU Fuel Channel Thermalhydraulics

ID Phenomenon

- FCT1 Convective Heat Transfer
- FCT2 Onset of Vapor/Void Generation
- FCT3 Pre-Critical Heat Flux (CHF) Boiling Heat Transfer

FCT4 Dryout (CHF)

- FCT5 Transition and Film Boiling
- FCT6 Quench and Rewet
- FCT7 Inter-Subchannel Single- and Two-Phase Mixing
- FCT8 Inter-Subchannel Turbulent Flow Scattering
- FCT9 Inter-Subchannel Diversion Cross-Flow
- FCT10 Phase Separation
- FCT11 Single-Phase and Two-Phase Density-Driven Flow
- FCT12 Single-Phase and Two-Phase Wall Shear and Form Losses
- FCT13 Radiative Heat Transfer
- FCT14 Steady-State and Transient Heat Conduction (Heat Diffusivity)
- FCT15 Non-Condensable Gas Effect
- FCT16 Zirconium/Steam and Zirconium/Air Thermal-Chemical Reaction
- FCT17 Fuel and Channel Deformation
- FCT18 Counter-Current Flow
- FCT19 Waterhammer
- FCT20 Flow Oscillations

ATTACHMENT

Excerpt from the Technical Basis Document^[5]

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1. Large Loss of Coolant Accident (LOCA)

2. Small Loss of Coolant Accident

- 2.1 Out-of-Core Breaks
 - 2.1.1 Pipe Breaks (Headers or Above)
 - 2.1.2 End Fitting Failure
 - 2.1.3 Stagnation Feeder Break
 - 2.1.4 Steam Generator Tube Rupture
- 2.2 In-Core Breaks
 - 2.2.1 Pressure Tube Rupture/Flow Blockage
 - 2.2.2 Inlet Feeder Breaks

3. Loss of Coolant Accident Coincident with Loss of Emergency Core Coolant Injection (LOCA\LOECI)

- 4. Secondary Side Breaks
- 5. Loss of Flow
- 6. Fuel Handling Failures
- 7. Loss of Regulation
- 8. Auxiliary System Failures
- 9. Atmospheric Dispersion

SECTION 1

TECHNICAL BASIS OF LARGE LOCA ANALYSES

1. INTRODUCTION

A large Loss of Coolant Accident (LOCA) involves a break in the heat transport system pressure boundary of sufficient magnitude that the normally operating reactivity control system, RRS, is incapable of maintaining reactivity balance and, as a result of the coolant void reactivity feedback, an immediate reactor power excursion occurs.

A large LOCA is characterized by the following general features:

- 1. an immediate power excursion driven by rapid coolant voiding in many channels,
- 2. a large rate of coolant discharge from the break into containment,
- 3. the potential for early impairment of fuel cooling, leading to possible pressure tube deformation,
- 4. the potential for fuel failures

- 5. a spike of iodine release from previously defected fuel into the coolant during the blowdown period
- 6. a potential increase in heat load to the moderator
- 7. the Emergency Coolant Injection System (ECIS) is available and coolant injection occurs.
- 8. an overpressure period in containment during which there can be a pressure driven release from containment.

The range of break sizes that are encompassed includes ones for which:

- the channels in the affected flow pass experience reduced flow in the normal flow direction (less than critical break size),
- channels in the affected core pass experience early, rapid reduction in flow to very low levels which are sustained for a limited duration (critical break size), and
- channels in the affected core pass experience sustained reverse flow during the blowdown (greater than critical break size).

2 KEY SAFETY CONCERNS

The safety concerns of relevance to large LOCA events whose consequences are quantified through the safety analysis are:

- · public and in-plant dose related to fission product releases from the fuel,
- · core coolable geometry related to fuel channel integrity, and
- containment integrity related to pressurization and hydrogen combustion.

3 ACCIDENT BEHAVIOUR

Quantification of the consequences associated with these safety concerns involves analysis of phenomena which can be grouped into sets of behaviour characterizing the physical processes that come into play during a large LOCA. These groups of behaviour typically evolve over limited time periods and proceed either in parallel with one another, or in a specific order determined by external sequences of events such as shutdown system initiation and ECIS initiation. For example, the early stages of blowdown cooling and the neutronic overpower transient evolve as parallel and inter-related behaviour, with the neutronic overpower transient behaviour occurring over a shorter time duration than blowdown cooling; whereas, ECIS delivery behaviour develops some tens of seconds following the neutronic overpower transient and the initial ECIS delivery proceeds in parallel with the later stages of blowdown cooling. Therefore, uncertainties in the modelling the phenomena associated with the different behaviour groupings are of relevance to the safety analysis only during those periods of time in which the behaviours exert a governing influence.

Phases of the Accident

The phases of a LOCA accident are defined according to the major time periods during the accident progression during which characteristic groups of behaviour are exhibited. For each of the major disciplines involved in a large LOCA the following phases are defined and the dominant behaviour during these phases are identified. Note that the time periods for each phase are approximate and do not imply specific limits on the start and end times for a phase.

Reactor Physics

1. Power Pulse (0-5 seconds) - the initial period following the break during which the reactor power increases due to positive coolant void feedback and which is terminated by shutdown system action. the dominant behaviour during this period is the *neutronic overpower transient*.

 Post shutdown (5 seconds onwards) - the period following reactor shutdown in which the reactor is brought subcritical, the spatial neutron flux distribution stabilizes and the power distribution becomes governed by decay heat.

System Thermalhydraulics / Fuel & Fuel Channel Thermal Mechanical Behaviour / Fission Product Release

- 1. Power Pulse (0-5 seconds) the initial period following the break during which the reactor power increases due to positive coolant void feedback and which is terminated by shutdown system action. the dominant behaviours during this period are *heat transport system depressurization*, *neutronic overpower transient and fuel heatup and axial fuel expansion*.
- 2. Early Blowdown Cooling (5 30 seconds) the period during which the heat transport system blowdown continues prior to ECIS initiation. The dominant behaviours during this period are heat transport system depressurization, blowdown cooling, fuel deformation, pressure tube deformation, fuel heatup, pressure tube heatup, fuel failure and fission product release.
- 3. Late Blowdown Cooling/ECIS Injection (30 200 seconds) the period of ongoing heat transport system blowdown with ECIS injection into the heat transport system. The dominant behaviours during this period are heat transport system depressurization, blowdown cooling, ECIS delivery, fuel deformation, pressure tube deformation, fuel heatup, pressure tube heatup and fission product release.
- 4. Refill (> 200 seconds) the period during which refill of channels in the core proceeds and a quasi-steady state is attained. The dominant behaviours during this period are, ECIS delivery, heat transport system refill, fuel cooling and fission product release.

